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## Elementary Fluid Mechanics CEE 357-02 Fall 2019- November 18 Exam 2

#### Circle the correct answer or fill in the blank

- 1. (**2pt**) The region where the velocity profile is constant, the wall shear is constant, and the pressure drops linearly with x (for either laminar and turbulent flow) is referred to as:
- (a) the entrance length
- (b) pipe entrance
- (c) fully developed flow region
- 2. (2pt) Laminar shear is dominant near
- (a) the intermediate region called the overlap layer
- (b) the region referred to as the wall layer
- (c) the region referred to as the outer layer
- 3. (**2pt**) The accepted design Re value for pipe flow transition to turbulent flow is taken to be\_\_\_\_\_(number value).

$$Re_{d,crit} = 2300$$

### Solve and show your work.

4. (24 pts) Seawater (30%) is flowing through a 40-cm pipe, 200 m long, with a head loss of 16 m at 20°C. The concrete pipe used to transmit the seawater is smoothed. Solve for the (a) final expected friction factor, (b) average velocity (m/s), and (c) flow rate (m³/s). (d) Plot the friction factor value on the Moody chart. Correct values will be accepted within 2% margin.

Concrete pipe (smoothed) roughness value ( $\epsilon$ ) = 0.04 mm Relative roughness ratio ( $\frac{\epsilon}{d}$ ) =  $\frac{0.04}{400}$  = 0.0001

$$f = h_f \frac{d^2g}{LV^2} = (16 m) \left(\frac{0.40 m}{200 m}\right) \left[\frac{2\left(9.81 \frac{m}{s^2}\right)}{V^2}\right]$$
 or  $fV^2 = 0.628 (SI units)$ 

Guess a f value to compute a value for velocity (V) from above:

$$V = \sqrt{0.628/f}$$

With a guess of 0.014 (similar to example and other homework problem guesses):

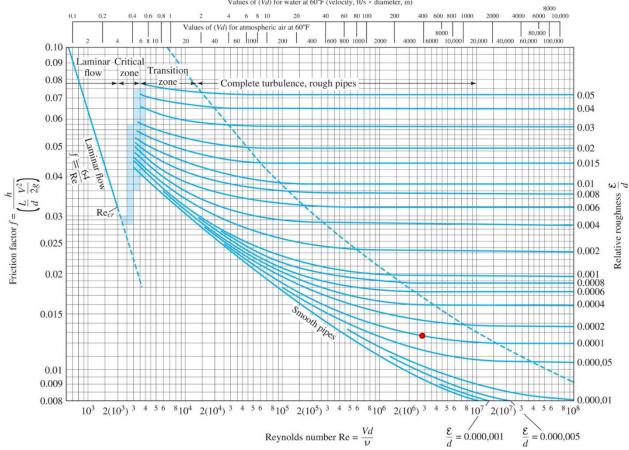
$$V = \sqrt{0.628/0.014} = 6.697 \, m/s$$

We calculate a Reynolds number (Red) using this V

$$Re_{d} = \frac{Vd}{v} = \frac{\rho_{Saltwater (30\%)}Vd}{\mu_{Saltwater (30\%)}} = \frac{\left(6.697 \frac{m}{s}\right) (0.40m)}{1.044 E - 6 m^{2}/s} = \frac{1025 kg/m^{3} \left(6.697 \frac{m}{s}\right) (0.40m)}{1.07 E - 3 kg/(m \cdot s)}$$

$$Re_{d} = 2.566.023$$

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Equation 6.48

$$\frac{1}{f^{1/2}} = -2.0 \log_{10} \left( \frac{\varepsilon/d}{3.7} + \frac{2.51}{Re_d f^{1/2}} \right) \qquad or \quad f = \left[ 1/\left( -2 \log_{10} \left( \frac{\varepsilon/d}{3.7} + \frac{2.51}{Re_d f^{1/2}} \right) \right) \right]^2$$

f= 0.01261  $\pm$  0.000252

Equation 6.49

$$\frac{1}{f^{1/2}} \approx -1.8 \log_{10} \left[ \frac{6.9}{Re_d} + \left( \frac{\varepsilon/d}{3.7} \right)^{1.11} \right] \qquad or \qquad f \approx \left[ 1 / \left( -1.8 \log_{10} \left[ \frac{6.9}{Re_d} + \left( \frac{\varepsilon/d}{3.7} \right)^{1.11} \right] \right) \right]^2$$

$$(a) \ f = 0.01259 \pm 0.000252 \tag{6pts}$$

(b) With a new f value of 0.01261 velocity can be updated:

$$V = \sqrt{0.628/0.01261} = 7.056 \frac{m}{s} \pm 0.141$$
 (6pts)

(c) Average flow rate (Q) m<sup>3</sup>/s:

$$Q = V\left(\frac{\pi}{4}\right)d^2 = 7.056\frac{m}{s} \times \left(\frac{\pi}{4}\right)(0.40m)^2 = 0.887\frac{m^3}{s} \pm 0.0177$$
 (6pts)

(d) Friction factor plotted above at f=0.0126, 
$$(\frac{\varepsilon}{d}) = \frac{0.04}{400} = 0.0001$$
, Re= 2,703,577 (6pts)

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	Circle the correct answer $\_$ is the dimensionless parameter used as an experimental value that relates n pipe resistance, thereby correlating head loss as proportional to $V^2$ .
(a) Darcy friction factor (b) Kármán constant (c) eddy viscosity	
6. ( <b>2 pt</b> ) A measure of a pknown as the	pipe's thickness and its resistance to stress caused by internal fluid pressure is
<ul><li>(a) Effective diameter ma</li><li>(b) Schedule No.</li><li>(c) Logarithm law</li></ul>	ss flow
• • •	lucts, we customarily replace a parameter in the head loss equation with an n-circular geometry which is referred to as
(a) the mixing length	

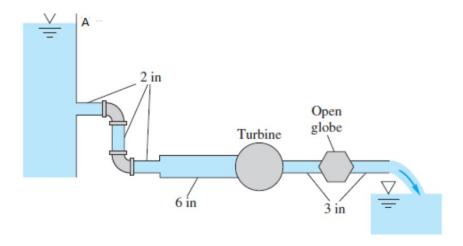
to

# Solve and show your work.

8. Minor losses in a pipe. (28 pts)

(b) the friction velocity(c) the hydraulic diameter

In the figure shown below there are 125 ft of 2-in pipe, 75 ft of 6-in pipe, and 150 ft of 3-in pipe, all new cast iron. There are two 90° elbows and an open globe valve, **all flanged**. If the exit elevation is zero and the elevation at A is 50 ft, what horsepower is extracted by the turbine (in hp) when the flow rate is 0.16 ft $^3$ /s of water at 20 °C? Hint: To save time use Haaland's formula to calculate f.



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Properties of water at 20°C,  $\rho$  = 1.94 slugs/ft<sup>3</sup>,  $\mu$  = 2.09E-5 slugs/(fts). Roughness ratio and L/d calculations for the three sections of the pipe are: (2pts)

$$2'' = \frac{\varepsilon}{d} = \frac{0.00085 ft}{\left(\frac{2}{12}\right) ft} = 0.0051$$

$$\frac{L}{D} = \frac{125 ft}{\left(\frac{2}{12}\right) ft} = 750$$

$$6'' = \frac{\varepsilon}{d} = \frac{0.00085 ft}{\left(\frac{6}{12}\right) ft} = 0.0017$$

$$\frac{L}{D} = \frac{75 ft}{\left(\frac{6}{12}\right) ft} = 150$$

$$3'' = \frac{\varepsilon}{d} = \frac{0.00085 ft}{\left(\frac{3}{12}\right) ft} = 0.0034$$

$$\frac{L}{D} = \frac{150 ft}{\left(\frac{3}{12}\right) ft} = 600$$

The velocities & Reynolds No.'s of the three pipes and f are determined using the following formula:

(2pts) (2pts) (2pts) 
$$V_1 = \frac{0.16}{\pi (2/12)^2/4} = 7.334 \frac{ft}{s} \; ; \qquad Re_1 = \frac{1.94 \; (7.33)(\frac{2}{12})}{2.09E-5} = 113500 \; ; \qquad f_1(Haaland) = 0.0314$$
 
$$V_2 = \frac{0.16}{\pi (6/12)^2/4} = 0.815 \frac{ft}{s} \; ; \qquad Re_1 = \frac{1.94 \; (0.815)(\frac{6}{12})}{2.09E-5} = 37819 \; ; \qquad f_2(Haaland) = 0.0264$$
 
$$V_3 = \frac{0.16}{\pi (3/12)^2/4} = 3.26 \frac{ft}{s} \; ; \qquad Re_1 = \frac{1.94 \; (3.26)(\frac{3}{12})}{2.09E-5} = 75639 \; ; \qquad f_3(Haaland) = 0.0286$$

$$K_1 = entrance = 0.5;$$
  $K_2 = 2$ " flanged 90° elbow = 0.39;  $K_3 = 2$ " flanged 90° elbow = 0.39;  $K_4 = expansion \approx 0.79;$   $K_5 = 3$ " open globe valve = 8.5 or 6.0 (or between);  $K_6 = exit = 1.0$  (2pts)

The turbine head equals the elevation difference minus losses, such that (with  $p_1=p_2=0$ , and  $V_1=V_2\approx 0$ ):

$$\frac{p_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \left(\frac{p_2}{\rho g} + \frac{V_2^2}{2g} + z_2\right) + \sum h_f + \sum h_m + h_{turbine}$$

$$h_{turbine} = (z_1 - z_2) - \sum h_f - \sum h_m = \Delta z - \frac{V_1^2}{2g} \left(f_1 \frac{L_1}{d_1} + \sum K\right) - \frac{V_2^2}{2g} \left(f_2 \frac{L_2}{d_2}\right) - \frac{V_3^2}{2g} \left(f_3 \frac{L_3}{d_3} + \sum K\right)$$

$$h_{turbine} = (50) - \frac{(7.33)^2}{2(32.2)} [0.0314(750) + 0.5 + 2(0.39) + 0.79] - \frac{(0.82)^2}{2(32.2)} (0.0264)(150)$$

$$- \frac{(3.26)^2}{2(32.2)} [(0.0287)(600) + 8.5 + 1]$$

$$h_{turbine} = (50) - \{[21.397] + (0.0411) + [4.408]\}$$

$$h_{turbine} = (50) - [25.847] = 24.153$$
 (10pts)

Thus, the resulting turbine power is determined using the following formula:

$$P_{turbine} = \rho g Q(h_{turbine}) = (62.4)(0.16)(24.15) = 241.15 \, ft \cdot \frac{lbf}{s} \div 550 \frac{ft \cdot lbf/s}{hp} = 0.438$$

The power extracted from the turbine is  $0.438 hp \pm 0.009$  (10pts)

### Circle the correct answer

- 9. (2 pt) Which of the following is NOT a common category of pumps:
- (a) Centrifugal
- (b) Impulse
- (c) Axial Flow
- 10. (2 **pt**) The *design flow rate Q\** is the flow rate at which
- (a) a pump provides its maximum discharge
- (b) a pump provides the highest possible head.
- (c) a pump provides its greatest efficiency.
- 11. (2 pt) This U.S. engineer invented the classical venturi device at Holyoke MA during development of the hydroelectric dam:
- (a) Giovani Venturi
- (b) Robert Manning.
- (c) Clemens Herschel

### Solve and show your work.

### 12. Turbomachinery (30 Pts)

A pump, geometrically similar to the 12.95-in model in the image shown below, has a diameter of 24 in and is to develop 32 hp at BEP when pumping gasoline (not water). Determine (a) the appropriate speed, in r/min, (b) the BEP head, in ft, and (c) the BEP flow rate, in gal/min. For gasoline,  $\rho = 680 \text{ kg/m}^3$ = 1.32 slug/ft<sup>3</sup>. Round the final answers to the nearest whole number.

From the given image, the BEP values are  $H_{1}=72 \text{ ft}$ ;  $Q_{1}=525 \text{ gal/min}$ ;  $\eta_{1}=0.80 \text{ gr}$ 

The power is determined using the following formula:

$$P_{1} = \rho g Q *_{1} H_{*1}/\eta = \left(1.94 \frac{slugs}{ft^{3}}\right) \left(32.2 \frac{ft}{s^{2}}\right) \left(525 \frac{gal}{min} \div 448.8 \frac{gal/min}{ft^{3}/s}\right) (72 ft)/0.8$$

$$= 6577 \frac{ft \cdot lbf}{s} = 11.96 hp$$
(6pts)

Use the scaling laws to find the new speed, head, and flow rate:

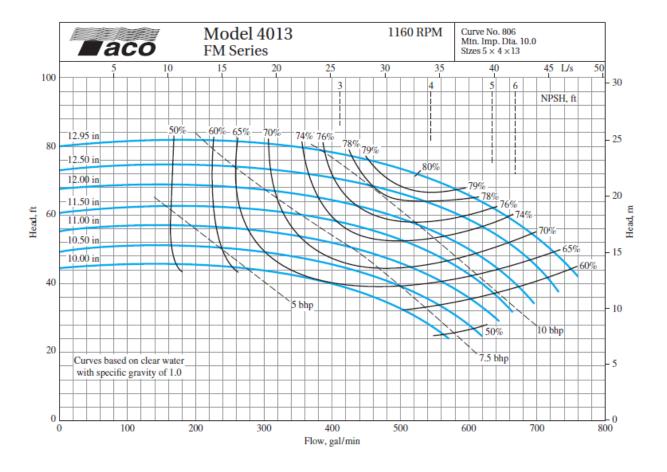
$$\frac{P_2}{P_1} = \frac{32}{11.96} = \left(\frac{\rho_2}{\rho_1}\right) \left(\frac{n_2}{n_1}\right)^3 \left(\frac{D_2}{D_1}\right)^5 = \left(\frac{1.32}{1.94}\right) \left(\frac{n_2}{1160}\right)^3 \left(\frac{24}{12.95}\right)^5, \quad solve \quad n_2 = 654.79 \ rpm \approx 655 \ rpm$$

$$\frac{H_2}{H_1} = \frac{H_2}{72} = \left(\frac{n_2}{n_1}\right)^2 \left(\frac{D_2}{D_1}\right)^2 = \left(\frac{654.8}{1160}\right)^2 \left(\frac{24}{12.95}\right)^2, \quad solve \quad H_2 = 78.8 \ ft \approx 79 \ ft$$
(8pts)

$$\frac{H_2}{H_1} = \frac{H_2}{72} = \left(\frac{n_2}{n_1}\right)^2 \left(\frac{D_2}{D_1}\right)^2 = \left(\frac{654.8}{1160}\right)^2 \left(\frac{24}{12.95}\right)^2, \qquad solve \quad H_2 = 78.8 \, ft \approx 79 \, ft \tag{8pts}$$

$$\frac{Q_2}{Q_1} = \frac{Q_2}{525} = \left(\frac{n_2}{n_1}\right) \left(\frac{D_2}{D_1}\right)^3 = \left(\frac{654.8}{1160}\right) \left(\frac{24}{12.95}\right)^3$$
, solve  $Q_2 = 1886.4 \approx 1886 \ gal/min$  (8pts)

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-----BONUS-----

Bonus (2 points): What is the difference between PDP pumps and dynamic (or momentum-change) pumps?

Dynamic pumps generally provide a higher flow rate than PDPs and a much steadier discharge but are ineffective in handling high-viscosity liquids. Dynamic pumps also generally need priming; if they are filled with gas, they cannot suck up a liquid from below into their inlet. The PDP on the other hand is self-priming for most applications. A dynamic pump can provide very high flow rates but usually with moderate pressure rises. In contrast a PDP can operate up to very high pressures but typically produces low flow rates.

Bonus (3 points): A pump from the family of Fig 11.8 (Non-dimensional plot of Performance) has D=28 in and n=18,000 r/min. Estimate the discharge (Q\*) for water at 60F ( density =1.94 slugs/ft<sup>3</sup>) at its best efficiency.

n = 18,000 r/min = 300 r/s

$$Q^* = C_Q n D^3 = (0.115)(300 \, r/s) \left(\frac{28in}{\frac{12in}{ft}}\right)^3 = 483.3 \frac{ft^3}{s} = 196,699 \, gal/min$$

Bonus (3 points): Calculate the "rigorous" specific speed (N') and the "quick/lazy" specific speed (N) for a family of pumps from Fig 11.8.

$$N_s' = \frac{C_{Q*}^{1/2}}{C_{H*}^{3/4}} = \frac{(0.115)^{1/2}}{(5.0)^{3/4}} = 0.104$$

$$N_s = 17,182 \, N_s' = 17,182 * (0.104) = 1740$$